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# Car radio Digital Signal Processor (DSP)

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## 1 FEATURES

### 1.1 Hardware

- Three 3rd-order Switched Capacitor Analog-to-Digital converters (SCADs)
- Digital-to-Analog Converters (DACs) with four times oversampling and noise shaping
- Digital stereo decoder for the FM multiplex signal
- Improved digital Interference Absorption Circuit (IAC) for FM
- Radio Data System (RDS) processing with an optional 16-bit buffer via a separate channel (two tuners possible)
- Auxiliary high Common-Mode Rejection Ratio (CMRR) analog CD input (CD-walkman, speech, economic CD-changer, etc.)
- I<sup>2</sup>C-bus controlled
- Four channel 5-band I<sup>2</sup>C-bus controlled parametric equalizer
- Two separate full I<sup>2</sup>S-bus and LSB-justified formats high performance input interfaces
- Audio output short-circuit protected
- Separate AM left and right inputs
- Phase-Locked Loop (PLL) to generate the high frequency DSP clock from a common fundamental oscillator crystal
- Analog single-ended tape inputs
- I<sup>2</sup>S-bus subwoofer output (mono or stereo)
- Expandable with additional DSPs for sophisticated features through an I<sup>2</sup>S-bus gateway
- Operating ambient temperature from -40 to +85 °C.

### 1.2 Software

- Improved FM weak signal processing
- Integrated 19 kHz MPX filter and de-emphasis
- Electronic adjustments: FM/AM level, FM channel separation and Dolby level
- Baseband audio processing (treble, bass, balance, fader and volume)
- Dynamic loudness or bass boost
- Audio level meter
- Tape equalisation (tape analog playback)



- Music Search System (MSS) detection for tape
- Dolby-B tape noise reduction
- Adjustable dynamics compressor
- CD de-emphasis processing
- Improved AM reception
- Soft audio mute
- AM IAC
- Pause detection for RDS updates
- Signal level, noise and multipath detection for AM/FM signal quality information.

## 2 APPLICATIONS

- Car radio systems.

## 3 GENERAL DESCRIPTION

The SAA7705H performs all the signal functions in front of the power amplifiers and behind the AM and FM multiplex demodulation of a car radio or the tape input.

These functions are:

- Interference absorption
- Stereo decoding
- RDS decoding
- FM and AM weak signal processing (soft mute, sliding stereo, etc.)
- Dolby-B tape noise reduction
- Audio controls (volume, balance, fader and tone).

Some functions have been implemented in the hardware (stereo decoder, RDS decoding and IAC for FM multiplex) and are not freely programmable. Digital audio signals from external sources with the Philips I<sup>2</sup>S-bus format or the LSB-justified 16, 18 or 20 bits format are accepted. There are four independent analog output channels. The channels have a hardware implemented 5-band parametric equalizer, controlled via the I<sup>2</sup>C-bus.

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- The DSP contains a basic program that enables a set with:
- AM/FM reception
  - Sophisticated FM weak signal functions
  - Music Search System (MSS) detection for tape
  - Dolby-B tape noise reduction system
  - CD play with compressor function
  - Separate bass and treble tone control and fader or balance control additional to the equalizers.

## 4 QUICK REFERENCE DATA

SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
<b>Supply</b>						
V <sub>DDD3V</sub>	digital supply voltage 3.3 V for DSP core	V <sub>DDD3Vx</sub> pins with respect to V <sub>SS</sub>	3	3.3	3.6	V
I <sub>DDD3V</sub>	supply current of the 3.3 V digital DSP core	high activity of the DSP at 27 MHz DSP frequency	–	80	110	mA
V <sub>DDD5V</sub>	supply voltage 5 V for periphery	V <sub>DDD5Vx</sub> pins with respect to V <sub>SS</sub>	4.5	5	5.5	V
I <sub>DDD5V</sub>	supply current of the 5 V digital periphery		–	3	5	mA
V <sub>DDA</sub>	analog supply voltage 3.3 V	V <sub>DDAx</sub> pins with respect to V <sub>SS</sub>	3	3.3	3.6	V
I <sub>DDA</sub>	analog supply current	zero input and output signal	–	40	50	mA
<b>Analog level inputs (AML and FML); T<sub>amb</sub> = 25 °C; V<sub>DDA1</sub> = 3.3 V; unless otherwise specified</b>						
S/N <sub>LAD</sub>	level-ADC signal-to-noise ratio	0 to 29 kHz bandwidth; maximum input level; unweighted	48	54	–	dB
V <sub>i(LAD)</sub>	input voltage level-ADC for full-scale		0	–	V <sub>DDA1</sub>	V
<b>Analog inputs; T<sub>amb</sub> = 25 °C; V<sub>DDA1</sub> = 3.3 V; unless otherwise specified</b>						
THD <sub>FMMPX</sub>	total harmonic distortion FMMPX input	input signal 0.35 V (RMS) at 1 kHz; bandwidth = 19 kHz; note 1	–	–70 0.03	–65 0.056	dB %
S/N <sub>FMMPX(m)</sub>	signal-to-noise ratio FMMPX input mono	input signal at 1 kHz; 0 dB reference = 0.35 V (RMS); bandwidth = 19 kHz; note 1	80	83	–	dB
S/N <sub>FMMPX(s)</sub>	signal-to-noise ratio FMMPX input stereo	input signal at 1 kHz; 0 dB reference = 0.35 V (RMS); bandwidth = 40 kHz; note 1	74	77	–	dB
THD <sub>CD</sub>	total harmonic distortion CD inputs	input signal 0.55 V (RMS) at 1 kHz; input gain = 1; bandwidth = 20 kHz	–	–83 0.007	–78 0.013	dB %
S/N <sub>CD</sub>	signal-to-noise ratio CD inputs	input signal at 1 kHz; 0 dB reference = 0.55 V (RMS); bandwidth = 20 kHz	81	84	–	dB
THD <sub>AM</sub>	total harmonic distortion AM inputs	input signal 0.55 V (RMS) at 1 kHz; bandwidth = 5 kHz	–	–80 0.01	–76 0.016	dB %

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SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
$S/N_{AM}$	signal-to-noise ratio AM inputs	input signal at 1 kHz; 0 dB reference = 0.55 V (RMS); bandwidth = 5 kHz	83	88	–	dB
$THD_{TAPE}$	total harmonic distortion TAPE inputs	input signal 0.55 V (RMS) at 1 kHz; bandwidth = 20 kHz;	–	–80 0.01	–76 0.016	dB %
$S/N_{TAPE}$	signal-to-noise ratio TAPE inputs	input signal at 1 kHz; 0 dB reference = 0.55 V (RMS); bandwidth = 20 kHz	81	83	–	dB
$V_{i(con)(max)(rms)}$	maximum conversion input level at analog inputs (RMS value)	THD < 1%	0.6	0.66	–	V

**Analog outputs;  $T_{amb} = 25\text{ °C}$ ;  $V_{DDA2} = 3.3\text{ V}$ ; unless otherwise specified**

$(THD + N)/S$	total harmonic distortion-plus-noise to signal ratio	output signal 0.72 V (RMS) at $f = 1\text{ kHz}$ ; $R_L > 5\text{ k}\Omega$ (AC); A-weighted	–	–75	–65	dB
DR	dynamic range	output signal –60 dB at 1 kHz; 0 dB reference = 0.77 V (RMS); A-weighted	92	102	–	dB
DS	digital silence	output signal at 20 Hz to 17 kHz; 0 dB reference = 0.77 V (RMS); A-weighted	–	–108	–102	dB

**Oscillator ( $f_{osc} = 11.2896\text{ MHz}$ )**

$f_{xtal}$	crystal frequency	–	11.2896	–	–	MHz
$f_{clk(DSP)}$	clock frequency DSP core	–	27.1656	–	–	MHz

**Note**

1. FMRDS and FMMPX input sensitivity setting '000' (see Table 17).

**5 ORDERING INFORMATION**

TYPE NUMBER	NAME	PACKAGE DESCRIPTION	VERSION
SAA7705H	QFP80	plastic quad flat package; 80 leads (lead length 1.95 mm); body 14 × 20 × 2.8 mm	SOT318-2

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### 6 BLOCK DIAGRAM

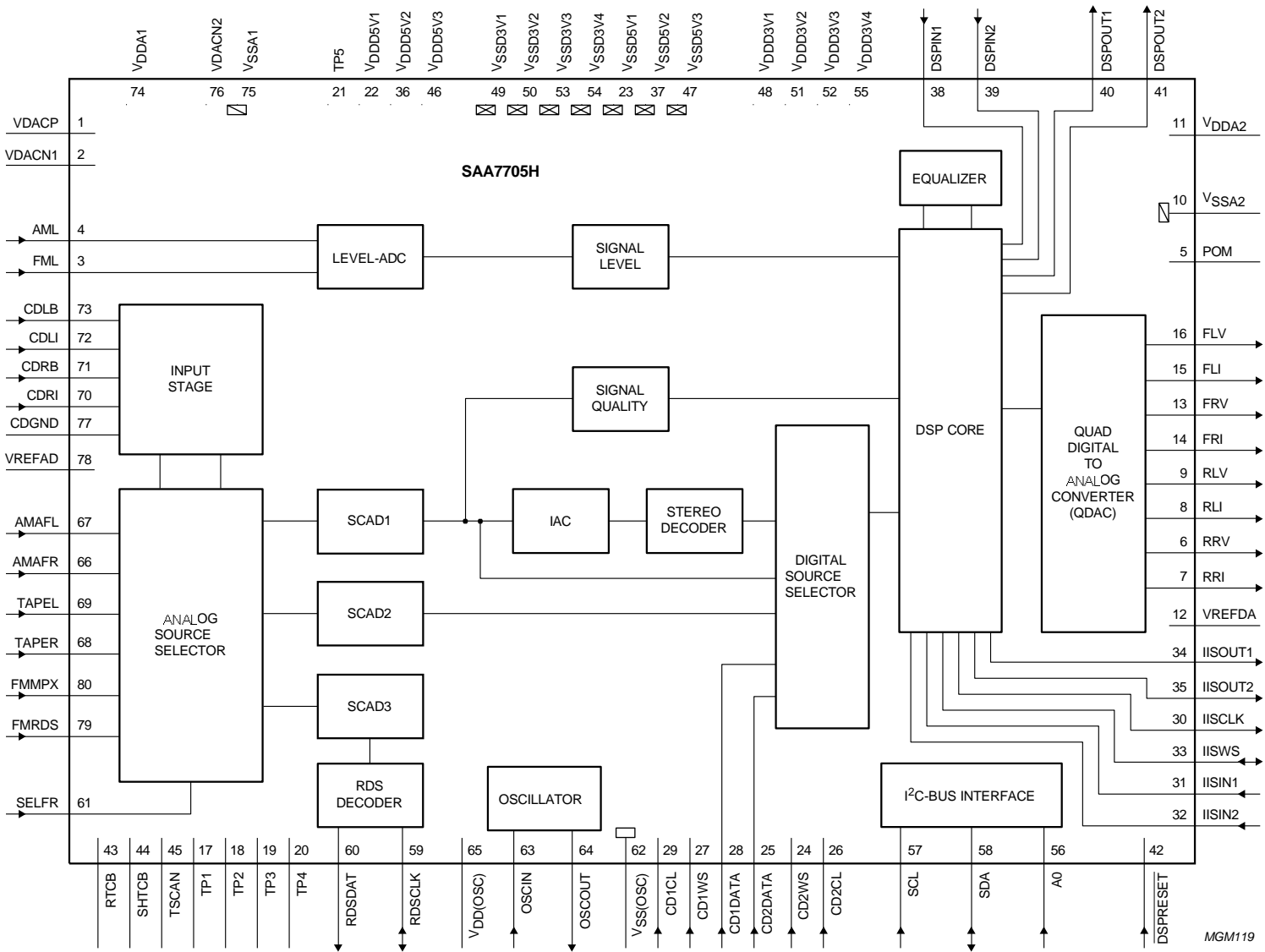


Fig.1 Block diagram.

MGM119

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## 7 PINNING

SYMBOL	PIN	PIN TYPE	DESCRIPTION
VDACP	1	AP2D	positive reference voltage for SCAD1, SCAD2, SCAD3 and level-ADC
VDACN1	2	AP2D	ground reference voltage 1 for SCAD1, SCAD2, SCAD3 and level-ADC
FML	3	AP2D	FM level input; via this pin the level of the FM signal is fed to the SAA7705H; the level information is needed for a correct functioning of the weak signal behaviour
AML	4	AP2D	AM level input; via this pin the level of the AM signal is fed to the SAA7705H
POM	5	AP2D	power-on mute of the QDAC; timing is determined by an external capacitor
RRV	6	AP2D	rear right audio voltage output of the QDAC
RRI	7	AP2D	rear right audio current output of the QDAC
RLI	8	AP2D	rear left audio current output of the QDAC
RLV	9	AP2D	rear left audio voltage output of the QDAC
V <sub>SSA2</sub>	10	APVSS	ground supply for the analog part of the QDAC
V <sub>DDA2</sub>	11	APVDD	positive supply for the analog part of the QDAC
VREFDA	12	AP2D	decoupling for voltage reference of the analog part of the QDAC
FRV	13	AP2D	front right audio voltage output of the QDAC
FRI	14	AP2D	front right audio current output of the QDAC
FLI	15	AP2D	front left audio current output of the QDAC
FLV	16	AP2D	front left audio voltage output of the QDAC
TP1	17	BT4CR	test pin, used in factory test mode, must not be connected
TP2	18	BT4CR	test pin, used in factory test mode, must not be connected
TP3	19	BT4CR	test pin, used in factory test mode, must not be connected
TP4	20	BT4CR	test pin, used in factory test mode, must not be connected
TP5	21	IBUFD	test pin, used in factory test mode, must be connected to V <sub>DD5V</sub>
V <sub>DD5V1</sub>	22	VDDE5	positive supply 1 for peripheral cells
V <sub>SS5V1</sub>	23	VSSE5	ground supply 1 for peripheral cells
CD2WS	24	IBUFD	word select input 2 from a digital audio source (I <sup>2</sup> S-bus or LSB-justified format)
CD2DATA	25	IBUFD	left or right data input 2 from a digital audio source (I <sup>2</sup> S-bus or LSB-justified format)
CD2CL	26	IBUFD	clock input 2 from a digital audio source (I <sup>2</sup> S-bus or LSB-justified format)
CD1WS	27	IBUFD	word select input 1 from a digital audio source (I <sup>2</sup> S-bus or LSB-justified format)
CD1DATA	28	IBUFD	left or right data input 1 from a digital audio source (I <sup>2</sup> S-bus or LSB-justified format)
CD1CL	29	IBUFD	clock input 1 from a digital audio source (I <sup>2</sup> S-bus or LSB-justified format)
IISCLK	30	BT4CR	clock output to extra DSP chip (I <sup>2</sup> S-bus)
IISIN1	31	IBUFD	data input channel 1 (front) from extra DSP chip (I <sup>2</sup> S-bus)
IISIN2	32	IBUFD	data input channel 2 (rear) from extra DSP chip (I <sup>2</sup> S-bus)
IISWS	33	BD4CR	word select input or output for extra DSP chip (I <sup>2</sup> S-bus)
IISOUT1	34	BD4CR	data output to extra DSP chip (I <sup>2</sup> S-bus)
IISOUT2	35	BD4CR	subwoofer output (I <sup>2</sup> S-bus)
V <sub>DD5V2</sub>	36	VDDE5	positive supply 2 for peripheral cells
V <sub>SS5V2</sub>	37	VSSE5	ground supply 2 for peripheral cells
DSPIN1	38	IBUFD	digital input 1 of the DSP core (flag F0 of the status register)
DSPIN2	39	IBUFD	digital input 2 of the DSP core (flag F1 of the status register)

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SYMBOL	PIN	PIN TYPE	DESCRIPTION
DSPOUT1	40	B4CR	digital output 1 of the DSP core (flag F2 of the status register)
DSPOUT2	41	B4CR	digital output 2 of the DSP core (flag F3 of the status register)
DSPRESET	42	IBUFU	reset input to the DSP core (active LOW)
RTCB	43	IBUFD	asynchronous reset test control block, connect to ground
SHTCB	44	IBUFD	shift clock test control block, connect to ground
TSCAN	45	IBUFD	scan control (active HIGH), connect to ground
V <sub>DD5V3</sub>	46	VDDE5	positive supply 3 for peripheral cells
V <sub>SS5V3</sub>	47	VSSE5	ground supply 3 for peripheral cells
V <sub>DD3V1</sub>	48	VDDI3	positive supply 1 for DSP core
V <sub>SS3V1</sub>	49	VSSI3	ground supply 1 for DSP core
V <sub>SS3V2</sub>	50	VSSI3	ground supply 2 for DSP core
V <sub>DD3V2</sub>	51	VDDI3	positive supply 2 for DSP core
V <sub>DD3V3</sub>	52	VDDI3	positive supply 3 for DSP core
V <sub>SS3V3</sub>	53	VSSI3	ground supply 3 for DSP core
V <sub>SS3V4</sub>	54	VSSI3	ground supply 4 for DSP core
V <sub>DD3V4</sub>	55	VDDI3	positive supply 4 for DSP core
A0	56	IBUFD	I <sup>2</sup> C-bus address selection
SCL	57	SCHMITCD	serial clock input (I <sup>2</sup> C-bus)
SDA	58	BD4SCI4	serial data input/output (I <sup>2</sup> C-bus)
RDSCLK	59	BD4CR	RDS bit clock output or RDS external clock input
RDSDAT	60	BT4CR	RDS data output
SELFR	61	IBUFD	AD input selection switch; to enable high-ohmic FMMPX input at fast tuner search on pin FMRDS; if SELFR is HIGH, the input at pin FMRDS is put through to SCAD1 and FMRDS gets high-ohmic; this pin works together with the AD register bit SELTWOTUN (see Table 9)
V <sub>SS(OSC)</sub>	62	APVSS	ground supply for crystal oscillator circuit
OSCIN	63	AP2D	crystal oscillator input: crystal oscillator sense for gain control or forced input in slave mode
OSCOUT	64	AP2D	crystal oscillator output: drive output to 11.2896 MHz crystal
V <sub>DD(OSC)</sub>	65	APVDD	positive supply for crystal oscillator circuit
AMAFR	66	AP2D	AM audio frequency analog input (right channel)
AMAFL	67	AP2D	AM audio frequency analog input (left channel)
TAPER	68	AP2D	tape analog input (right channel)
TAPEL	69	AP2D	tape analog input (left channel)
CDRI	70	AP2D	CD analog input (right channel)
CDRB	71	AP2D	feedback input of the CD analog input (right channel)
CDLI	72	AP2D	CD analog input (left channel)
CDLB	73	AP2D	feedback input of the CD analog input (left channel)
V <sub>DDA1</sub>	74	APVDD	analog positive supply for SCAD1, SCAD2, SCAD3 and level-ADC
V <sub>SSA1</sub>	75	APVSS	analog ground supply SCAD1, SCAD2, SCAD3 and level-ADC
VDACN2	76	AP2D	ground reference voltage 2 for SCAD1, SCAD2, SCAD3 and level-ADC

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SYMBOL	PIN	PIN TYPE	DESCRIPTION
CDGND	77	AP2D	positive reference for analog CD block
VREFAD	78	AP2D	common-mode reference voltage SCAD1, SCAD2, SCAD3 and level-ADC
FMRDS	79	AP2D	FM RDS analog input
FMMPX	80	AP2D	FM multiplex analog input

**Table 1** Explanation of pin types

PIN TYPE	DESCRIPTION
AP2D	analog input/output
APVDD	analog supply
APVSS	analog ground
VDDE5	5 V peripheral supply
VSSE5	5 V peripheral ground connection, no connection to the substrate
VDDI3	3.3 V supply to digital core and internal I/O pads
VSSI3	3.3 V ground to digital core and internal I/O pads, no connection to the substrate
SCHMITCD	CMOS, Schmitt trigger input with active pull-down
IBUFU	CMOS, active pull-up to all VDDE5 pads
IBUFD	CMOS, active pull-down to all VSSE5 pads
BD4CR	bidirectional CMOS I/O buffer, 4 mA, slew rate control
BT4CR	4 mA CMOS 3-state output buffer, slew rate control
B4CR	4 mA CMOS output buffer, slew rate control
BD4SCI4	CMOS I/O pad with open-drain output



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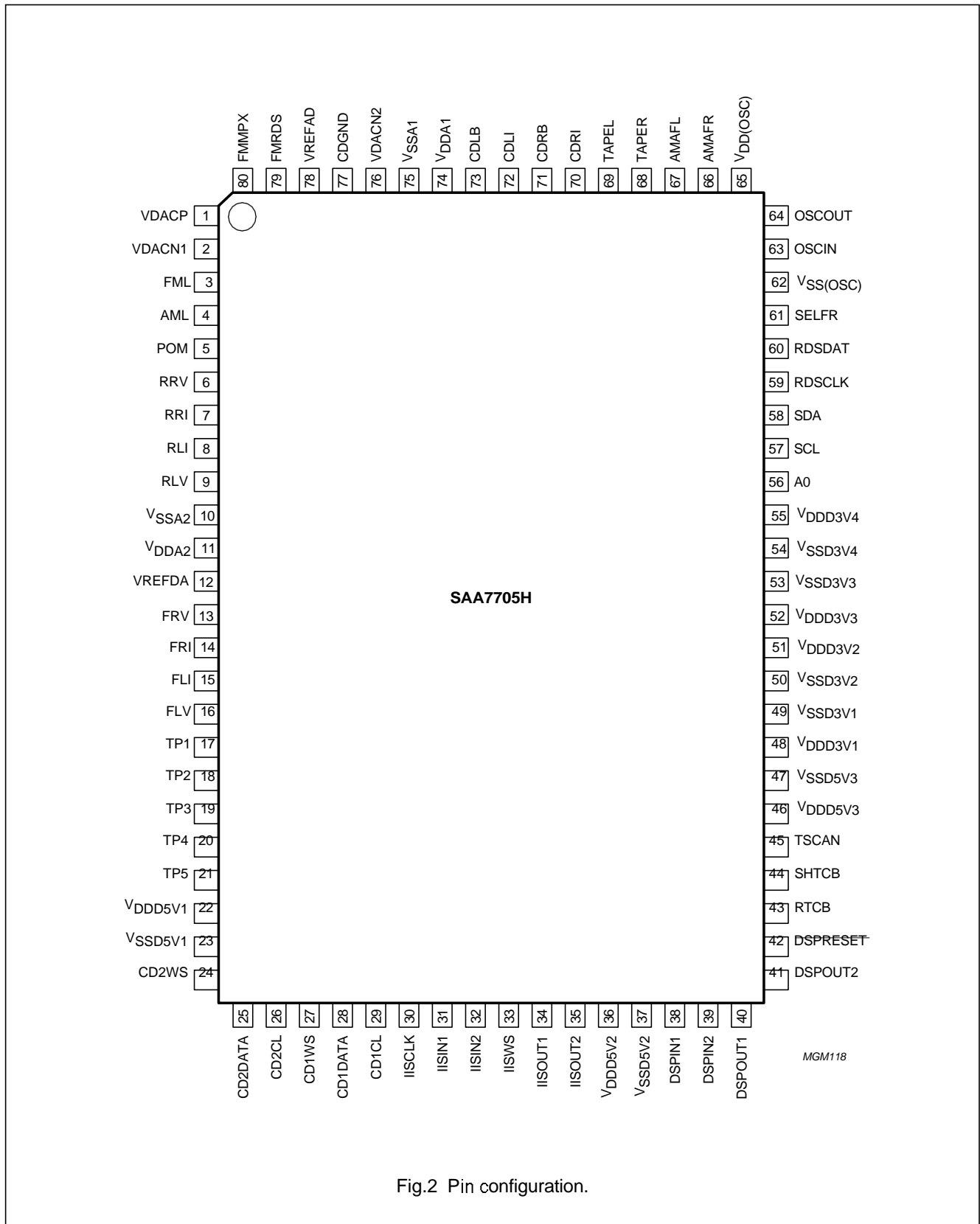


Fig.2 Pin configuration.

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### 8 FUNCTIONAL DESCRIPTION

The SAA7705H consists of a DSP core and periphery. The DSP core is described in Sections 8.6, 8.7 and 8.11. The periphery handles the following tasks:

- FM and level information processing (see Section 8.1)
- Analog source selection and analog-to-digital conversion of the analog audio sources (see Section 8.2)
- Digital-to-analog conversion of the DSP output QDAC (see Section 8.3)
- Clock circuit and oscillator (see Section 8.4)
- Equalizer accelerator circuit (see Section 8.5)
- I<sup>2</sup>C-bus interface (see Section 8.8 and Chapter 12)
- RDS decoder (see Section 8.10).

#### 8.1 FM and level information processing

##### 8.1.1 SIGNAL PATH FOR LEVEL INFORMATION

For FM weak signal processing and for AM and FM purposes (absolute level and multipath), an FM level and an AM level input is implemented (pins FML and AML). In the case of radio reception clocking of the filters and the level-ADC is based on a 38 kHz sample frequency. The DC input signal is converted by a bitstream first-order Sigma-Delta ADC followed by a decimation filter.

The input signal has to be obtained from the radio part. Two different configurations for AM and FM reception are possible:

- A circuit with two separate level signals: one for FM level and one for AM level
- A combined circuit with AM and FM level information on the FM level input.

The level input is selected with bit LEVAM-FM of the SEL register (see Table 12 and Chapter 12).

##### 8.1.2 SIGNAL PATH FROM FMMPX INPUT TO IAC AND STEREO DECODER

The SAA7705H has four analog audio source channels. One of the analog inputs is the FM multiplex signal. Selection of this signal can be achieved by the SEL register bits AUX-FM and CD-TAPE (see Table 12). The multiplexed FM signal is converted to the digital domain in SCAD1, a bitstream third-order SCAD. The first decimation with a factor of 16 takes place in down sample filter ADF1. This decimation filter can be switched by means of the SEL register bit WIDE-NARROW (see Table 12) in the wide or narrow band position. In case

of FM reception, it must be in the narrow position.

The FMMPX path is followed by the sample-and-hold switch of the IAC (see Section 8.1.5) and the 19 kHz pilot signal regeneration circuit. A second decimation filter reduces the output of the IAC to a lower sample rate. One of the two filter outputs contains the multiplexed signal with a frequency range of 0 to 60 kHz.

The outputs of this signal path to the DSP (which are all running on a sample frequency of 38 kHz) are:

- Pilot presence indication: Pilot-I. This one bit signal is LOW for a pilot frequency deviation <4 kHz and HIGH for a pilot frequency deviation >4 kHz and locked on a pilot tone.
- FM reception stereo signal. This is the 18-bit output of the stereo decoder after the matrix decoding in Information System Network (ISN) I<sup>2</sup>S-bus format. This signal is fed via a multiplexer to a general I<sup>2</sup>S-bus interface block that communicates with the DSP core.
- A noise level indication. This signal is derived from the first MPX decimation filter via a wide band noise filter. Detection is done with an envelope detector. This noise level is filtered in the DSP core and is used to optimize the FM weak signal processing.

##### 8.1.3 INPUT SENSITIVITY FOR FM AND RDS SIGNALS

The FM and RDS input sensitivity is designed for tuner front ends which deliver an output voltage varying from 65 to 225 mV (RMS) at a sweep of 22.5 kHz for a 1 kHz tone. The intermediate standard input sensitivities can be reached in steps of 1.6 dB, to be programmed with the AD register bits VOLFM and VOLRDS (see Tables 9 and 17). The volume control of the FMMPX and the FMRDS input can be controlled separately. VOLFM and VOLRDS = 000 is the most sensitive position, VOLFM and VOLRDS = 111 the least sensitive position. Due to the analog circuit control of the volume gain, the input impedance of pin FMMPX or pin FMRDS changes with the volume setting.

##### 8.1.4 AD INPUT SELECTION SWITCH

Pin SELFR makes it possible to change to another transmitter frequency with the same radio program to assess the quality of that signal. In case of a stronger transmitter signal the decision can be made by the software to switch to the new transmitter. The FMMPX input is normally used to process the FM signal. This FMMPX input is connected via a relative large capacitor to the MPX tuner output. Switching the tuner to another transmitter frequency means another DC voltage level on the MPX output of the tuner and a charging of the

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series capacitor (because the FMMPX input of the SAA7705H is low-ohmic). Pulling SELFR HIGH during such an update, causes the FMMPX input to become high-ohmic, preventing charging of the capacitor. The signal probing of the new transmitter quality is done via the FMRDS input.

### 8.1.5 INTERFERENCE ABSORPTION CIRCUIT

The Interference Absorption Circuit (IAC) detects and suppresses ignition interference. This hardware IAC is a modified, digitized and extended version of the analog circuit which is in use for many years already.

The IAC consists of an MPX mute function switched by mute pulses from two ignition interference pulse detectors. A third detector inhibits muting.

The three detectors are:

- **Interference detector:** The input signal of the first detector is the output signal of SCAD1. This interference detector analyses the high frequency contents of the MPX signal. The discrimination between interference pulses and other signals is performed by a special Philips patented fuzzy logic such as algorithm and is

based on probability calculations. This detector performs optimally with higher antenna voltages. On detection of ignition interference, this logic will send appropriate pulses to the MPX mute switch.

- **Level detector:** The input signal of the second detector is the FM level signal (the output of the level-ADC). This detector performs optimally with lower antenna voltages. It is therefore complementary to the first detector. The characteristics of both ignition interference pulse detectors can be adapted to the properties of different FM front ends by means of the coefficients in the IAC register and the level-IAC register (see Section 12.4). Both IAC detectors can be switched on or off independently. Both IAC detectors can mute the MPX signal independently.
- **Dynamic detector:** The third detector is the dynamic IAC circuit. This detector switches off the IAC completely if the frequency deviation of the FM multiplex signal is too high. The use of narrow band IF filters can result in AM modulation. This AM modulation could be interpreted by the IAC circuitry as interference caused by the car's engine.

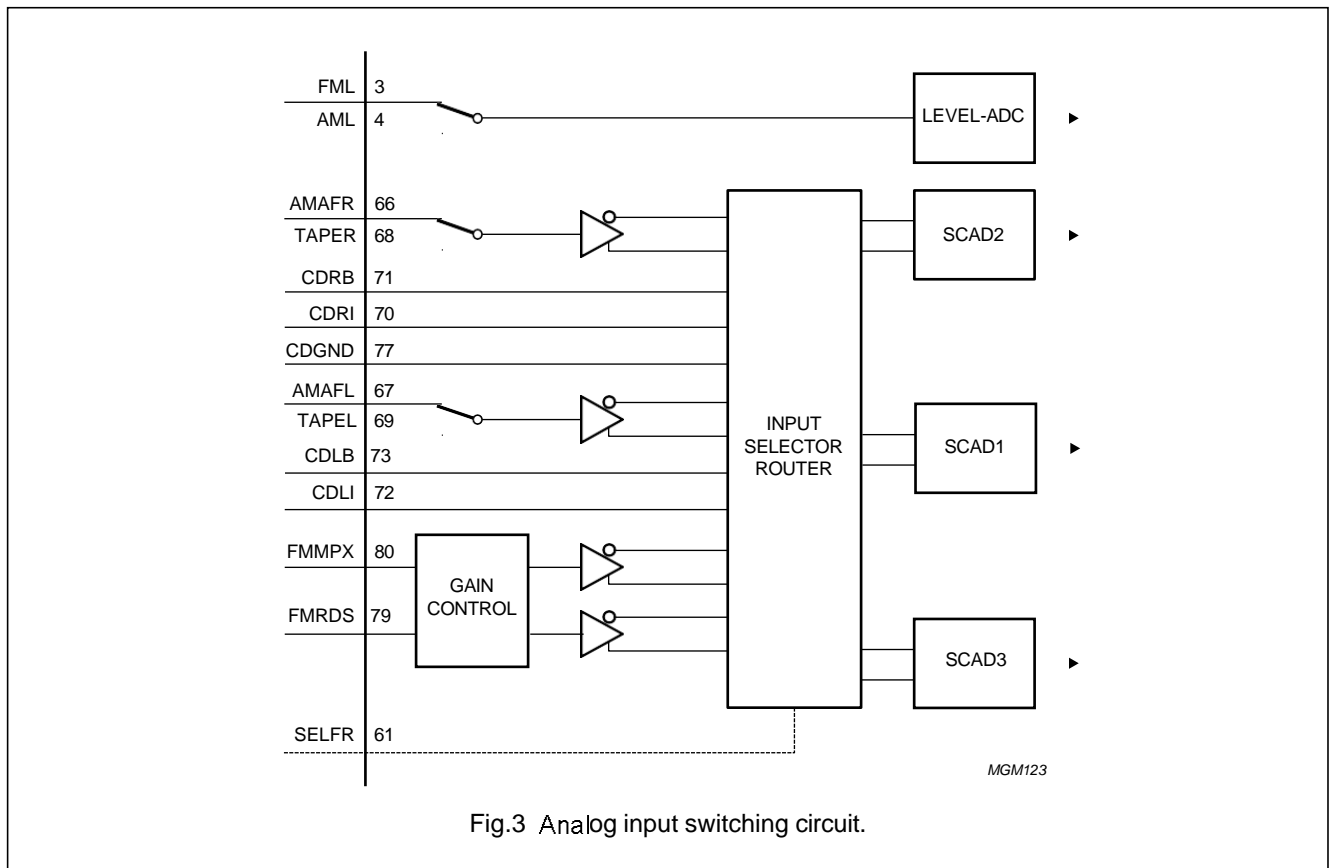


Fig.3 Analog input switching circuit.

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Parameter setting for the IAC detectors is done by means of 5 different coefficients. Upon reset, the nominal setting for a good performing IAC detector is selected.

### 8.1.5.1 AGC set point (1 bit)

In case the sensitivity and feed-forward factor are out of range in a certain application, the set point of the AGC can be shifted. The set point controls the sensitivity of the other IAC control parameters. See bit 11 of the IAC register (Table 11).

### 8.1.5.2 Threshold sensitivity offset (3 bits)

With this parameter the threshold sensitivity of the comparator in the interfering pulse detectors can be set. It also influences the amount of unwanted triggering. Settings are according to Table 25.

### 8.1.5.3 Deviation feed-forward factor (3 bits)

This parameter determines the reduction of the sensitivity of the detector by the absolute value of the MPX signal. This mechanism prevents the detector from unwanted triggering at noise with modulation peaks. In Table 24 the possible values are given.

### 8.1.5.4 Suppression stretch time (3 bits)

This parameter sets the duration of the pulse suppression after the detector has stopped sending a trigger pulse. It can be switched off by setting the value '000'. The duration can be selected in steps of one period of the 304 kHz (3.3  $\mu$ s) sample frequency. In Table 23 the possible values are given.

### 8.1.5.5 MPX delay (2 bits)

With this parameter the delay time between 2 and 5 samples of the 304 kHz sample frequency can be selected. The needed value depends on the used front end of the car radio. Settings are according to Table 22.

### 8.1.5.6 Level-IAC threshold (4 bits)

With this parameter the sensitivity of the comparator in the ignition interference pulse detector can be set. It also influences the amount of unwanted triggering. The possible values are given in Table 21. The prefix value '0000' switches off the level-IAC function.

### 8.1.5.7 Level-IAC feed-forward setting (2 bits)

This parameter allows for adjusting delay differences in the signal paths from the FM antenna to the MPX mute, namely, via the FM level-ADC and level-IAC detection and

via the FM demodulator and MPX conversion and filtering. These differences depend on the front end used in the car radio. With a simultaneous appearance of a peak disturbance at the FM level input and the MPX ADC input of the IC, a zero delay setting takes care for the level-IAC mute pulse to coincide with the passage of the disturbance in the MPX mute circuit. The setting for the level-IAC feed-forward allows to advance the mute pulse by 1 sample period or to delay it by 1 or 2 sample periods of the 304 kHz clock, with respect to the default value. The appropriate register bits for each setting are given in Table 20.

### 8.1.5.8 Level-IAC suppression stretch time (2 bits)

This parameter sets the time that the mute pulse is stretched when the FM level input has stopped exceeding the threshold. The duration can be selected in steps of one period of the 304 kHz (3.3  $\mu$ s) sample frequency. In Table 19 the possible values are given.

### 8.1.5.9 Dynamic IAC threshold levels

If enabled by bit 15 of the LEVELIAC register, this block will disable temporarily all IAC actions if the MPX mono signal exceeds a threshold deviation (threshold 1) for a given time with a given excess amount (threshold 2). This MPX mono signal is separated from the MPX signal with a low-pass filter with the -3 dB corner point at 15 kHz. The possible values of this threshold are given in Table 18.

### 8.1.5.10 IAC testing mode

The internal IAC trigger signal is visible on pin DSPOUT2 if bit IACTRIGGER of the IAC register is set. In this mode the effect of the parameter settings on the IAC performance can be verified.

## 8.2 Analog source selection and analog-to-digital conversion

### 8.2.1 INPUT SELECTION SWITCHES

In Fig.3 the block diagram of the input is shown. The input selection is controlled by bits in the input selector control register and the input selection pin SELFR. The relationship between these bits and the switches is indicated in Table 26.

### 8.2.2 SIGNAL FLOW OF THE AM, ANALOG CD AND TAPE INPUTS

The signal of the two single-ended stereo AM inputs can be selected by the correct values of the SEL register bits according to Table 26.

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The AM and the TAPE inputs are buffered with an operational amplifier to ensure a high-impedance input which enables the use of an external resistor divider for signal reduction. For correct biasing of the first operational amplifier a resistor must be connected between the input and pin VREFAD, which acts as a virtual ground (see Fig.21). The analog input switching circuit is shown in Fig.3. The input for an analog CD player is explained in more detail in Section 8.2.3.

### 8.2.3 THE ANALOG CD BLOCK

Special precautions are taken to realize a high Common-Mode Rejection Ratio (CMRR) in case of the use of a CD player output processed via analog inputs. The block diagram is shown in Fig.4. The operational amplifiers OAR and OAL are used as buffers. The gain of these operational amplifiers can be adjusted via the external resistors and is in this case 0.54 by using a 8.2 kΩ and a 15 kΩ resistor.

The reference inputs of these operational amplifiers are connected to a separate pin CDGND. This pin is on one side AC connected to the ground shielding of the cable coming from the CD player and via a resistor >1 MΩ to pin VREFAD. In this configuration the common-mode signal propagates all the way to the SCAD block inputs of SCAD1 and SCAD2. The SCADs themselves have a good rejection ratio for in-phase common-mode signals.

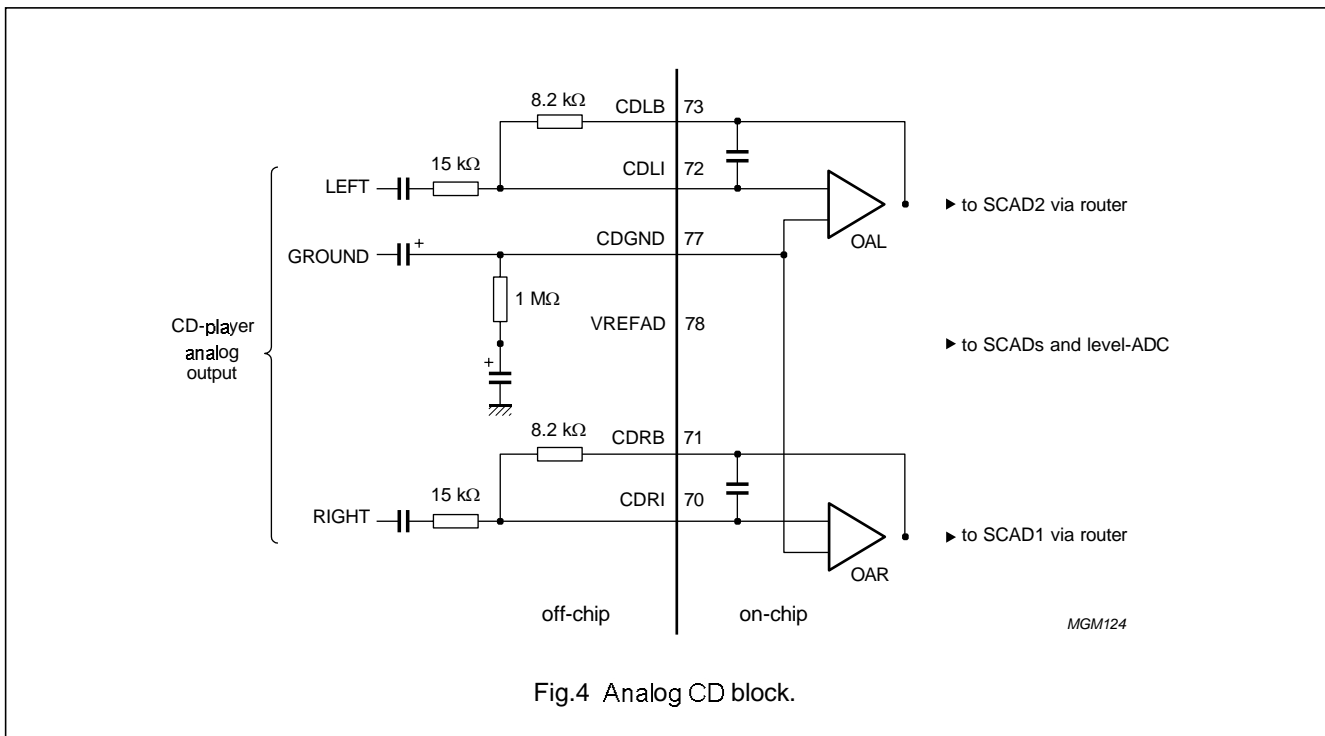
Which part of the common-mode signal is processed as the real input signal depends on the ratio of the CDGND resistor and the series resistor in the cable and the difference in input offset of the operational amplifiers. The induced signals on the CDLI and CDRI lines are of the same amplitude and therefore rejected as common-mode signals in the SCADs.

### 8.2.4 PIN VREFAD

The middle reference voltage of the SCAD1, SCAD2, SCAD3 and level-ADC can be filtered via this pin. This voltage is used as half the supply reference of the SCAD1, SCAD2, SCAD3 and as the positive reference for the level-ADC and buffers. External capacitors (connected to VSSA1) prevent crosstalk between the SCADs and buffers and improve the power supply rejection ratio of all blocks. This pin must also be used as a reference for the inputs AMAFL, AMAFR, TAPEL, TAPER and CDGND.

### 8.2.5 PINS VDACN1, VDACN2 AND VDACP

These pins are used as ground and positive supply reference for the SCAD1, SCAD2, SCAD3 and the level-ADC. For optimal performance, pins VDACN1 and VDACN2 must be directly connected to the VSSA1 and pin VDACP to the filtered VDDA1.



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### 8.2.6 SUPPLY OF THE ANALOG INPUTS

The analog input circuit has separate power supply connections to allow maximum filtering of the analog supply voltages:  $V_{SSA1}$  for the analog ground and  $V_{DDA1}$  for the analog supply.

### 8.3 Analog outputs

#### 8.3.1 DACs

Each of the four low noise high dynamic range DACs consists of a 15-bit signed magnitude DAC with current output, followed by a buffer operational amplifier. For each of the four audio output channels a separate converter is used. Each converter output is connected to the inverting input of one of the four internal CMOS operational amplifiers. The non-inverting input of this operational amplifier is connected to the internal reference voltage. Together with an internal resistor the conversion of current-to-voltage of the audio output is achieved.

#### 8.3.2 UPSAMPLE FILTER

To reduce spectral components above the audio band, a fixed 4 times oversampling and interpolating 18-bit digital IIR filter is used. It is realized as a bit serial design and consists of two consecutive filters. The data path in these filters is 22 bits to prevent overflow and to maintain a

signal-to-noise ratio larger than 105 dB. The word clock for the upsample filter ( $4 \times f_s$ ) is derived from the audio source timing. If the internal audio source is selected, the sample frequency can be either 44.1 or 38 kHz. In case of external digital sources (CD1 and CD2), a sample frequency from 32 to 48 kHz is possible.

#### 8.3.3 VOLUME CONTROL

The total volume control has a dynamic range of more than 100 dB (0 dB being maximal input on the I<sup>2</sup>S-bus input). With the signed magnitude noise shaped 15-bit DAC and the internal 18-bit registers (these registers provide the digital data communication between the DSP and the QDAC) of the DSP core a useful digital volume control range of 100 dB is possible by calculating the corresponding coefficients.

The step size is freely programmable and an additional analog volume control is not needed in this design. The SNR of the audio output at full-scale is determined by the total 15 bits of the converter. The noise at low outputs is fully determined by the noise performance of the DAC. Since it is a signed magnitude type, the noise at digital silence is also low. The disadvantage is that the total THD is higher than conventional DACs. The typical THD-plus-noise versus output level is shown in Fig.5.

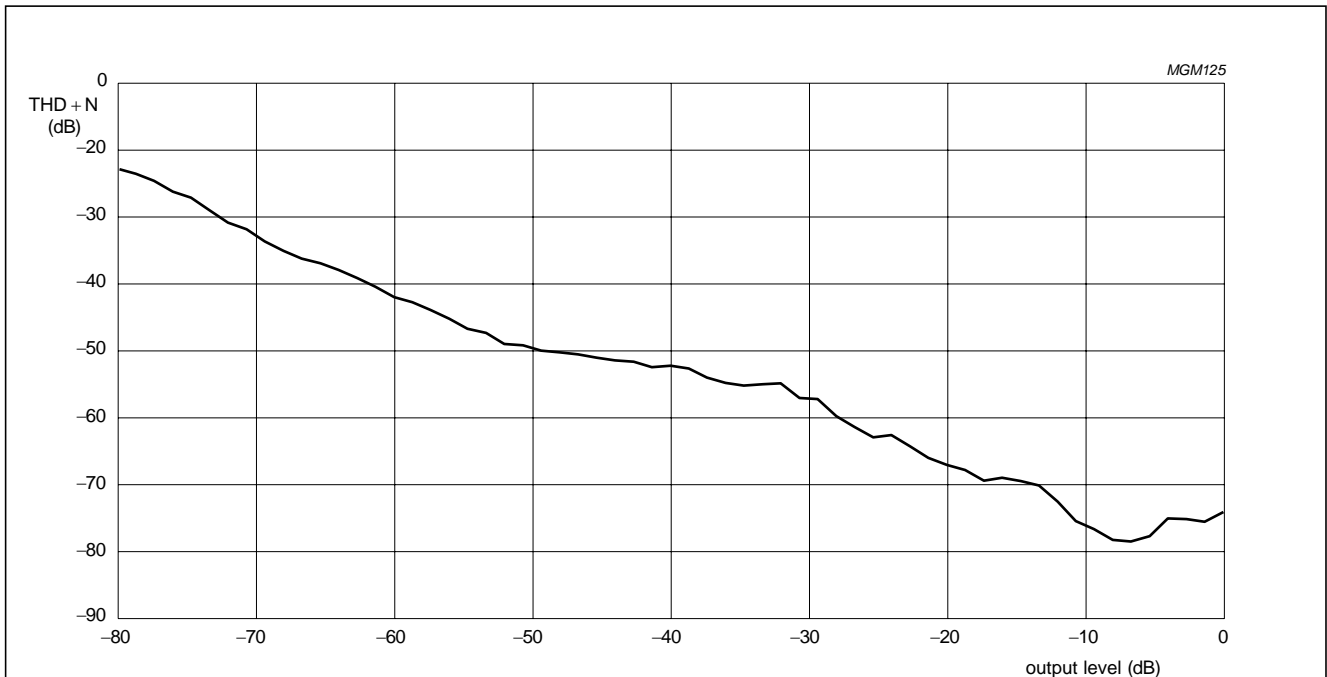


Fig.5 Typical THD + N curve versus output level.

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### 8.3.4 FUNCTION OF PIN POM

With pin POM it is possible to switch-off the reference current of the DAC. The capacitor on pin POM (see Fig.21) determines the time after which this current has a soft switch-on. At power-on, the current audio signal outputs are always muted. The external capacitor is loaded in two stages via two different current sources. The loading starts at a current level that is 9 times lower than the load current after the voltage on pin POM has risen above 1 V. This results in an almost dB-linear behaviour. However, the DAC has an asymmetrical supply and the DC output voltage will be half the supply voltage under functional conditions. During start-up the output voltage is not defined as long as the supply voltage is below the threshold voltages of the transistors. A small jump in DC is possible at start up. In this DC jump audio components can be present.

### 8.3.5 POWER-OFF PLOP SUPPRESSION

To avoid plops in a power amplifier, the supply voltage (3.3 V) for the analog part of the DAC can be supplied from the 5 V supply via a transistor. A capacitor is connected to  $V_{DDA2}$  to maintain power to the analog part if the 5 V supply is switched off fast. In this case the output voltage will decrease gradually allowing the power amplifier some extra time to switch-off without audible plops.

### 8.3.6 THE INTERNAL PIN VREFDA

Using two internal resistors, half of the supply voltage  $V_{DDA2}$  is obtained and coupled to an internal buffer. This reference voltage is used as a DC voltage for the output operational amplifiers and as a reference for the DAC. In order to obtain the lowest noise and to have the best ripple rejection, a capacitor has to be connected between this pin and ground.

### 8.3.7 INTERNAL DAC CURRENT REFERENCE

As a reference for the internal DAC current and also for the DAC current source output, a current is drawn from pin VREFDA to  $V_{SSA2}$  (ground) via an internal resistor. The value of this resistor determines also the DAC current (absolute value). Consequently, the absolute value of the current varies from device to device due to the spread of the reference resistor value. This, however, has no influence on the absolute output voltages because these voltages are derived from a conversion of the DAC current to the actual output voltage via internal resistors.

### 8.3.8 SUPPLY OF THE ANALOG OUTPUTS

All the analog circuitry of the DACs and the operational amplifiers are powered by 2 pins:  $V_{DDA2}$  and  $V_{SSA2}$ .  $V_{DDA2}$  must have sufficient decoupling to prevent high THD and to ensure a good Power Supply Rejection Ratio (PSRR). The digital part of the DAC is fully supplied from the DSP core supply.

## 8.4 Clock circuit and oscillator

The device has an on-chip oscillator. The block diagram of this Pierce oscillator is shown in Fig.6. The active element needed to compensate for the loss resistance of the crystal is the block  $G_m$ . This block is placed between the external pins OSCIN and OSCOUT. The gain of the oscillator is internally controlled by the AGC block. A sine wave with a peak-to-peak voltage close to the oscillator power supply voltage is generated. The AGC block prevents clipping of the sine wave and therefore the generation of harmonics as much as possible. At the same time the voltage of the sine wave is as high as possible which reduces the jitter going from the sine wave to the clock signal.

### 8.4.1 SUPPLY OF THE CRYSTAL OSCILLATOR

The supply of the oscillator is separated from the other supplies. This minimizes the feedback from the ground bounce of the chip to the oscillator circuit. Pin  $V_{SS(OSC)}$  is used as ground and pin  $V_{DD(OSC)}$  as positive supply.

### 8.4.2 THE PHASE-LOCKED LOOP CIRCUIT TO GENERATE THE DSP CLOCK AND OTHER DERIVED CLOCKS

A PLL circuit is used to generate the DSP clock and other derived clocks.

The minimum equalizer clock frequency is  $480f_s$ . If  $f_s$  equals 44.1 kHz, this results in a minimum oscillator frequency of 21.1687 MHz. Crystals for the crystal oscillator in the range of twice the required DSP clock frequency (approximately 40 MHz) are always third-overtone crystals and must be manufactured on customer demand. This makes these crystals expensive. The PLL enables the use of a commonly available crystal operating in fundamental mode. For this circuit a 11.2896 MHz ( $256 \times 44.1$  kHz) crystal is chosen. This type of crystal is widely used.

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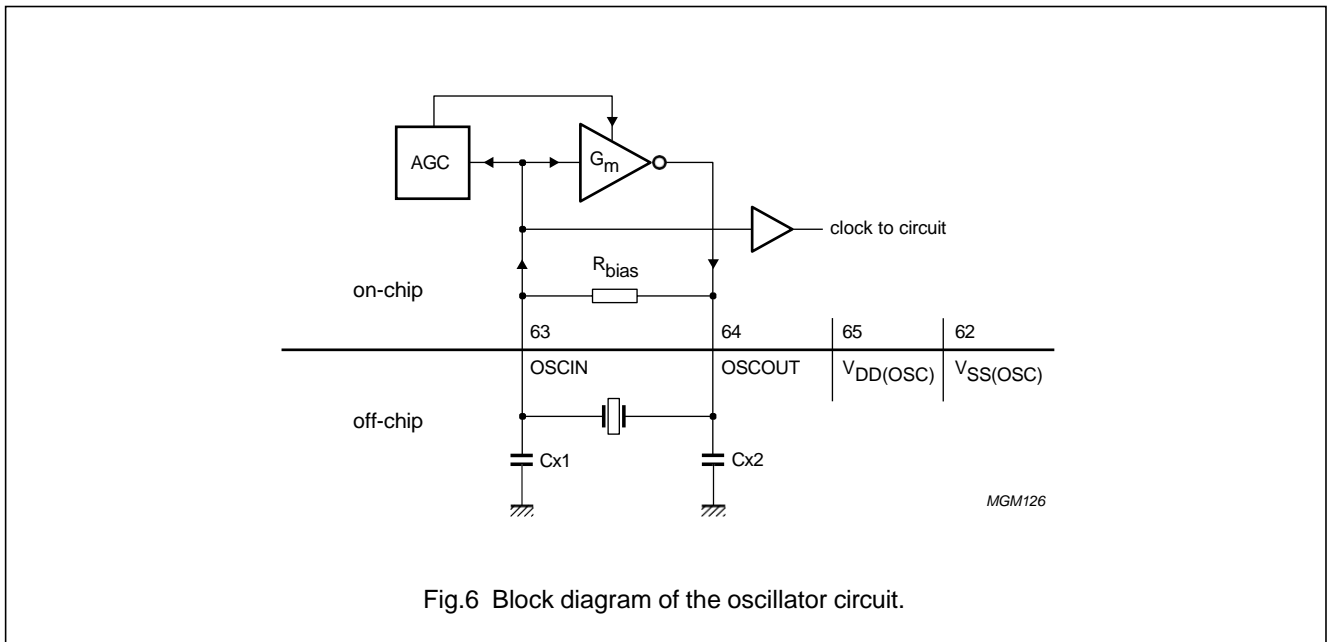


Fig.6 Block diagram of the oscillator circuit.

Although multiples of the crystal frequency of 11.2896 MHz fall within the FM reception band, this will not disturb the reception. The relatively low frequency crystal is driven in a controlled way and the resonating crystal produces harmonics of a very low amplitude in the FM reception band.

The block diagram of the programmable PLL is shown in Fig.7. The oscillator is used in a fundamental mode. The 11.2896 MHz oscillator frequency is divided by 256 and the resulting signal is fed to the phase detector as a reference signal. The base for the clock signal is a current controlled oscillator (free running frequency 70 to 130 MHz).

After having been divided by 4, the required clock frequency for the DSP core is available. To close the loop this signal is further divided by 4 and by the PLL clock division factor N. N can be programmed with the DCSCTR register bits PLL-DIV (see Tables 7 and 15) in the range from 93 to 181. This provides some flexibility in the choice of the crystal frequency.

With the recommended crystal, N = 154 and the DSP clock frequency ( $f_{DSP}$ ) equals 27.1656 MHz. N = 154 is the default position at start-up. By setting the AD register bit DSPTURBO (see Tables 9 and 15), the PLL output frequency, and consequently  $f_{DSP}$ , can be doubled. This feature is not used in the proposed application.

The clock frequency of the PLL oscillator divided by two ( $2f_{DSP}$ ) is also used as the clock for the DCS block.

8.4.3 THE CLOCK BLOCK

For the digital stereo decoder a clock signal is needed which is the 512-multiple of the pilot tone frequency of the FM multiplex signal. This is done by the Digitally Controlled Sampling (DCS) block, which generates this  $512 \times 19 \text{ kHz} = 9.728 \text{ MHz}$  clock, the DCS clock, by locking to the pilot frequency. This block is also able to generate other frequencies. It is controlled by the DCSCTR and DCSDIV registers (see Tables 7 and 8). Default settings of the DCS and the PLL guarantee correct functioning of the DCS block.

8.4.4 SYNCHRONIZATION WITH THE CORE

In case of I<sup>2</sup>S-bus input the system can run on audio sample frequencies of  $f_s = 32 \text{ kHz}$ ,  $38 \text{ kHz}$ ,  $44.1 \text{ kHz}$  or  $48 \text{ kHz}$ . After processing of an input sample, the Input flag (I-flag) of the status register (see Section 8.7) of the DSP core is set to logic 1 during 4 clock cycles on the falling edge of the internal or external I<sup>2</sup>S-bus WS pulses. This flag can be tested with a conditional branch instruction in the DSP. This synchronisation starts in parallel with the input signal due to the short period that the I-flag is set. It is obvious that the higher  $f_s$  the lower the number of cycles available in the DSP program.



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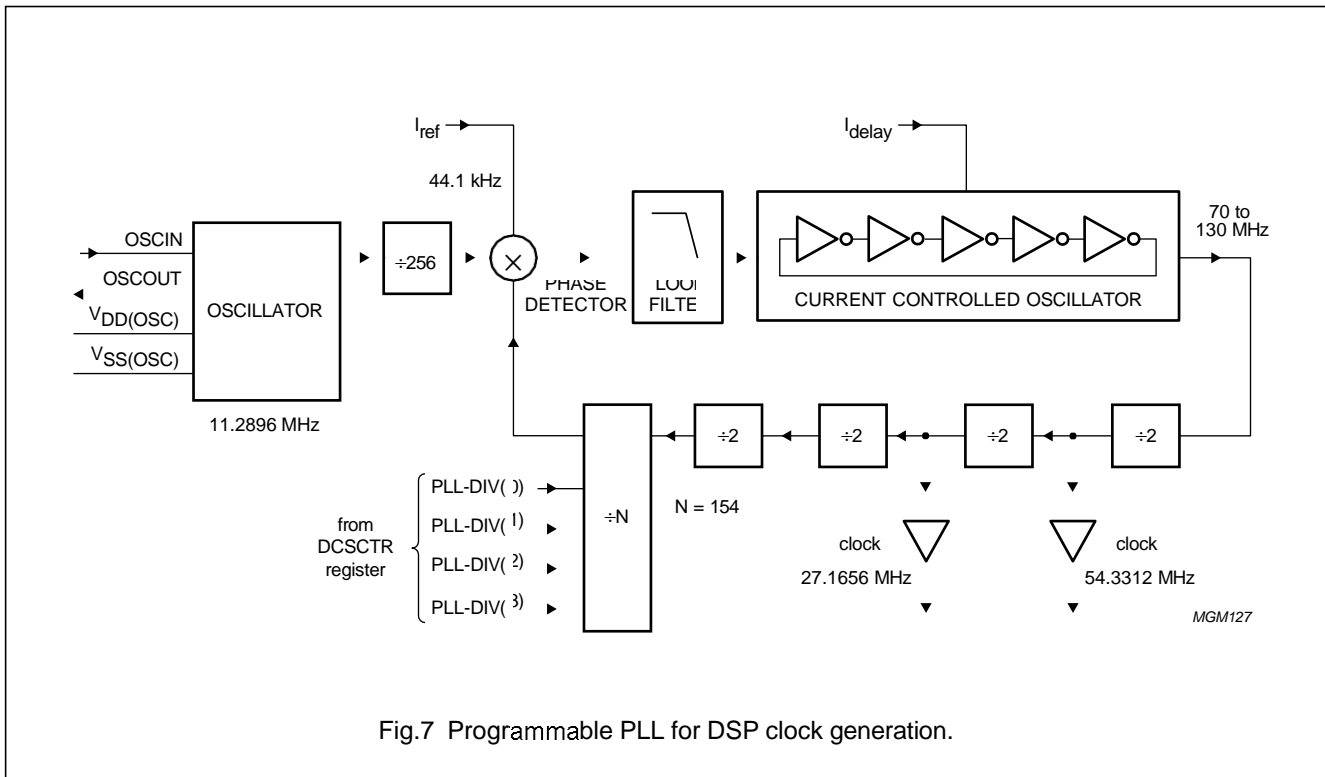


Fig.7 Programmable PLL for DSP clock generation.

8.5 Equalizer accelerator circuit

8.5.1 INTRODUCTION

The Equalizer accelerator (EQ) circuit is an equalizer circuit used as a hardware accelerator to the DSP core. Its inputs and outputs are stored in registers of the DSP core (these registers provide the digital data communication between the equalizer and the DSP core). The flag that starts the DSP program, refreshes the EQ input and output registers and starts the EQ controller.

The EQ circuit contains one second-order filter data path that is twenty-fold multiplexed. With this circuit, a two-channel equalizer of 10 second-order sections per channel or a four-channel equalizer of 5 second-order sections per channel can be realized.

The centre frequency, gain and Q-factor of all 20 second-order sections can be set independently from each other. Every section is followed by a variable attenuation of 0 or 6 dB. Per section, 4 bytes are needed to store the settings. During an audio sample period, all settings are read as 16-bit words in 80 read accesses to the coefficient memory.

8.5.2 EQ CIRCUIT OVERVIEW

This EQ circuit contains the following parts:

- A second-order filter data path, with programmable coefficients and with 40 state registers, supporting storage of the two filter states for 20 multiplexed filters; this part is clocked by a gated clock
- Signal routing around this filter data path, consisting of:
  - buses and selectors to configure the 20 filter sections for two or four channels;
  - input and output registers, with proper interfacing with the DSP core and with conversions between parallel and serial formats.
- A coefficient memory, to be loaded via the I<sup>2</sup>C-bus interface
- A controller, started by the write pulse for input and output registers, that controls the signal routing, controls the clock for the filter data path, addresses the coefficient memory and controls its programming.

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